

Detection Method For Phase-Modulated Symbols With A Correlator-Bank

Cross-Reference To Related Application

This application claims priority of European Patent Application No. 00310290.2, which was filed on November 20, 2000.

The invention relates to a method for the detection of a symbol from a received signal wherein the symbol is a selected symbol out of a predetermined set of symbols, wherein each symbol of the predetermined set is a CCK symbol comprising a sequence of chips wherein each of the chips is PSK-modulated according to a selected modulation code wherein each of the selected modulation codes comprises a first sub-modulation code which is a selection from a plurality of first sets of predetermined phase modulating elements and a second sub-modulation code which is a selection from one second set of predetermined phase modulating elements wherein at least one of said predetermined phase modulating elements of said second set is a complex value such as defined in the high speed IEEE 802.11b standard, wherein a modulation code is selected from said modulation codes which correlates according to a correlation method with the received signal.

The invention also relates to an apparatus for the detection of a symbol from a received signal wherein the symbol is a selected symbol out of a predetermined set of symbols, wherein each symbol of the predetermined set is a CCK symbol comprising a sequence of chips wherein each of the chips is PSK-modulated according to a selected modulation code wherein each of the selected modulation codes comprises a first sub-modulation code which is a selection from a plurality of first sets of predetermined phase modulating elements and a second sub-modulation code which is a selection from one second set of predetermined phase modulating elements wherein at least one of said predetermined phase modulating elements of said second set is a complex value such as defined in the high speed IEEE 802.11b standard, the apparatus comprising correlating means for correlating the received signal with said modulation codes according to a correlation method and means for selecting a modulation code from said modulation codes on the basis of the correlation.

Methods and apparatus of this type are known in practice. Usually methods and apparatus of this type use a bank of correlators which is employed in the receiver. On the basis of the correlation results with the received signal, which is performed in the bank of correlators, the symbol of the received signal can be detected. For this detection the output of each correlator is the input argument of a mathematical function. The

mathematical function is maximum for the correlator corresponding to the maximum function. According to said method and apparatus, which uses a pre-determined set of symbols, the symbol detection can be performed in such a way that it minimizes sensitivity to noise in the received signal.

5 Examples of possible pre-determined sets of symbols are given in the high speed standard in the IEEE 802.11b standard. This IEEE 802.11b standard is especially meant for the 2.4 [GHz] band, also called Industrial Scientific Medical Band (ISMB-band), in the United States. It is noticed that corresponding bands are available in most other regions in the world. Users
10 have free access to the ISMB-band if they comply with the standards of the standard proposal. A first important issue of the standard proposal is that the each used symbol has a relatively flat frequency power spectrum, which minimises risks of jamming fellow-users. A second important issue of the IEEE 802.11b standard is that not all possible symbols in the pre-determined set of
15 symbols are used. This results in a redundant and robust detection mechanism.

A first disadvantage of the known methods and apparatus for the detection of a symbol of a received signal is the large number of correlators which are used in the correlator-bank. A second disadvantage of the type of
20 known methods and apparatus is the large processing power which is required for performing the mathematical function, which function is used for the selection of a correlator in the correlator-bank, and operates on the complex output of each of the correlators. This mathematical function normally calculates the length of complex input argument, which leads to at least two
25 multiplications per correlator. In order to reduce the processing power several approximations of said mathematical function have been proposed. However, these approximations only yields sub-optimal detection performance.

It is an object of the invention to realise a reduction of the number of correlators in the correlation- bank. It is also an object of the invention to
30 reduce the required processing power for the evaluation of said mathematical function. Furthermore it is an object of the invention to obtain an optimal detection performance. More in particular it is an object of the invention to offer a detection method which, despite the reduction in the number of correlators and the reduction in the required processing power of the
35 mathematical function, yields the performance of a maximum likelihood detection method. Finally, the invention seeks a method having the

advantages stated above which can be used for receive-signals which comply with IEEE 802.11. For this, the method according to the invention is characterised in that the method comprises at least the following steps:

- a. correlating the received signal with each of the possible first sub-modulation codes for obtaining first correlation results and selecting a correlation result;
- b. phase-modulating the selected first correlation result with one of said possible second sub-modulation codes for each possible second sub-modulation code for obtaining second correlation results;
- c. selecting the maximum second correlation result from the second correlation results;
- d. selecting the symbol of the received signal on the basis of a combination the first and second correlating results.

In the method according to the invention two main parts of the correlation method can be distinguished. In the first part the first correlation results are determined and in the second part the second correlation results are determined. The second correlation results are obtained by rotating one selected first correlation result to several positions in the complex plane. Since the second part only comprises processing of one selected first correlation result this yields a reduction in required processing power compared with a situation wherein each first correlation result has to be rotated in the complex plane.

A further embodiment of the method according to the invention is characterised in that in step a. for each first correlation result the value of a function of the correlation result is determined and subsequently the first correlation result which provides the maximum value of the function is selected wherein the function is determined by the type of modulation of the second sub-modulation code. Preferably the function is a function of the real and/or imaginary parts of the first correlation result. The evaluation of this function requires less processing power than conventional functions wherein the length of a complex correlation result is calculated, while still leading the optimal Maximum Likelihood Detection symbol.

In an advantageous embodiment of the method of the invention the number of first modulation results obtained in step a. equals to $C_1 * C_2 * \dots * C_{i-1} * C_i * C_{i+1} * \dots * C_n$ wherein C_i is the number of elements of the i^{th} first set of the first sets, and preferably the number of second modulation results obtained in

step c. equals the number of predetermined phase modulating elements of the second set.

A further embodiment of the method of the invention is characterised in that in step b in a first substep the selected first correlation
 5 result is phase-modulated with each of said possible second sub-modulation codes and in a second substep real values are determined from results obtained in the first substep for obtaining the second correlation results.

In an embodiment according to the invention in step c. a predetermined phase modulating element of the second set is selected which
 10 provides the selected second correlation result, and in step d. the predetermined phase modulating elements of the first sets are selected which provide the selected first correlation result. A further embodiment of the method is characterised in that the selected predetermined phase modulating elements of the second set and the predetermined phase modulating elements
 15 of the first sets are combined to obtain the symbol of the received signal.

In an advanced embodiment of the method of the invention in step a. a first correlator bank comprising a number of correlators is used, wherein this number of correlators equals the number of first correlation results, and in
 20 step b. a second correlator bank is used which comprises a number of correlators, wherein this number of correlators equals the number of second correlation results.

The apparatus according to the invention is characterised in that the apparatus comprises the following means:

- a first correlator bank for correlating the received signal with each
 25 of the possible first sub-modulation codes for obtaining first correlation results;
- first selection means for selecting a first correlation result from the first correlation results;
- a second correlator bank for phase-modulating the first correlation result with one of said possible second sub-modulation codes for each possible
 30 second sub-modulation code for obtaining second correlation results;
- second selection means for selecting the maximum second correlation result from the second correlation results;
- a control-unit comprising means for controlling the first selecting means on the basis of the first correlation results;
- 35 third selecting means for selecting the symbol of the received signal on the basis of the first and second correlation results.

In a favourable embodiment of the apparatus of the invention the third selection means select a predetermined phase modulating element of the second set which provides the selected second correlation result and also select predetermined phase modulating elements of the first sets which provide the selected first correlation results. Preferably the third selection means of the apparatus of the invention combine the selected predetermined phase modulating element of the second set and the selected predetermined phase modulating elements of the first sets to obtain the symbol in the received signal.

In the accompanying drawings, in which certain modes of carrying out the present invention are shown for illustrative purposes:—

Figure 1 is diagram schematically showing an embodiment of an apparatus according to the invention for the detection of a symbol from a received signal;

Figure 2 is a schematic example of a symbol from a received signal;

Figure 3 is a co-ordinate system in the complex plane illustrating a second sub-modulation code for the chips in the symbol of figure 2.

An embodiment of an apparatus 2 for the detection of a symbol from a received signal according to the invention is schematically shown in figure 1.

The apparatus 2 comprises a first correlator bank 4 for obtaining first correlation results 6.m ($m=1,2,\dots,M$) on the basis of an input signal 8 and first selection means 10 for selecting one of the first correlation results.

Furthermore the apparatus 2 comprises a second correlator bank 12 which receives the selected first correlation result 14 and generates second

correlation results 16.k ($k=1,2,\dots,K$). The apparatus 2 also comprises second selection means 18 for selecting one of the second correlation results, a control unit 20 for controlling the first selection means 10 and third selection means 22 for selecting the detection symbol. The third selection means 22 select the detection symbol on the basis of the selected first correlation result 6.m

corresponding to the correlator 24.m in the first correlator bank 4 and the selected second correlation result 16.k corresponding to the correlator 26.k in the second correlator bank 12. The third selection means receives an input signal 28 comprising information about the selected correlator 24.m and an input signal 30 comprising information about the selected correlator 26.k, the output signal 32 comprises information about the detection symbol from the received signal 8. The first selection means 10 comprises a kind of a switch

which can connect the output of one correlator of any correlator 24.m
(m=1,2,...,M) to the second correlator bank 12. The switch 34 is controlled with
the control signal 36 on the basis of the first correlation results 6.m
(m=1,2,...,M).

5 The symbol from the received signal 8 is a selected symbol out of a
predetermined set of symbols wherein each symbol of the predetermined set is
a Complementary Coded Keying symbol (short: CCK-symbol). A CCK-symbol
comprises a sequence of chips wherein each of the chips is Phase Shift Keying
10 modulated (short: PSK-modulated). The PSK-modulation is based on a selected
modulation code wherein each of the selected modulation codes comprises a
first sub-modulation code which is a selection from a plurality of first sets of
predetermined phase modulating elements and a second sub-modulation code
which is a selection from one second set of predetermined phase modulating
15 elements. At least one of said predetermined phase-modulating elements of the
second sets is a complex value.

Figure 2 presents an example of a symbol 38, out of a predetermined
set of symbols, comprising eight chips 40 wherein each chip is phase
modulated. This phase modulation is defined with the complex numbers s_1 up
to s_8 . With these complex numbers the symbol 38 can be written in vector
20 notation as $\mathbf{s}=[s_1, s_2, \dots, s_8]^T$. An example of a set of high speed CCK-symbols 38
is given in the high speed IEEE 802.11b standard according to:

$$\mathbf{s} = [e^{j(\varphi_1+\varphi_2+\varphi_3+\varphi_4)}, e^{j(\varphi_1+\varphi_3+\varphi_4)}, e^{j(\varphi_1+\varphi_2+\varphi_4)}, \\ -e^{j(\varphi_1+\varphi_4)}, e^{j(\varphi_1+\varphi_2+\varphi_3)}, e^{j(\varphi_1+\varphi_3)}, -e^{j(\varphi_1+\varphi_2)}, e^{j(\varphi_1)}]^T, \quad (\text{I})$$

25 wherein j is a complex number and wherein the predetermined phase
modulating elements $e^{j\varphi_1}, e^{j\varphi_2}, e^{j\varphi_3}, e^{j\varphi_4}$ can take on a set of predetermined
values. The predetermined phase modulating elements are divided in three
first sets and one second set. The three first sets contain the predetermined
phase modulating elements $e^{j\varphi_2}, e^{j\varphi_3}, e^{j\varphi_4}$ and the second set contains the
30 predetermined phase modulating element $e^{j\varphi_1}$.

The three first sets of predetermined phase modulating elements are
respectively defined according to:

$$e^{j\varphi_2}, \text{ with } \langle . \rangle \\ e^{j\varphi_3}, \text{ with } \langle \langle . \rangle \rangle \quad (\text{IIA})$$

$$e^{j\varphi_4}, \text{ with } \langle\langle\langle.\rangle\rangle\rangle$$

wherein $\varphi_2, \varphi_3, \varphi_4$ are the phase parameters of the respective predetermined phase modulating elements. The phase parameters define the possible values of the respective phase modulating elements. The phase parameters can only take on one value out of a limited set of values. For the high speed IEEE

802.11b standard this set is defined according to $\langle\varphi_1 \in \left\{0, \frac{\pi}{2}, -\pi, -\frac{\pi}{2}\right\}\rangle$,

$$\langle\langle\varphi_2 \in \left\{0, \frac{\pi}{2}, -\pi, -\frac{\pi}{2}\right\}\rangle\rangle,$$

$$\langle\langle\langle\varphi_3 \in \left\{0, \frac{\pi}{2}, -\pi, -\frac{\pi}{2}\right\}\rangle\rangle\rangle$$

The so-called 5.5 Mbit/s fallback rate corresponds to a different set which set is defined with (IIB):

$$\begin{aligned} &\langle\varphi_2 \in \left\{\frac{\pi}{2}, -\frac{\pi}{2}\right\}\rangle, \\ &\langle\langle\varphi_3 \in \{0\}\rangle\rangle, \\ &\langle\langle\langle\varphi_4 \in \{0, \pi\}\rangle\rangle\rangle. \end{aligned} \quad (\text{IIB})$$

The predetermined phase modulating element in the second set is defined by:

$$e^{j\varphi_1}, \quad (\text{IIIA})$$

wherein φ_1 is a phase parameter. The phase parameter φ_1 can take on one value out of the following set of values:

$$\varphi_1 \in \left\{0, \frac{\pi}{2}, -\pi, -\frac{\pi}{2}\right\} \quad (\text{IIIB})$$

The modulation codes of the set of CCK-symbols follow from the value combinations of the phase modulating elements from the first sets (II) and the second set (III). From equation (I) it follows that the phase modulating element $e^{j\varphi_1}$ is a common element for all chips of the symbol (I).

The modulation code of the symbol (I) is divided in a first sub-modulation code and a second modulation code. The first sub-modulation code s_1 is defined in terms of the predetermined phase modulating elements of the first sets according to:

$$\mathbf{s}_1 = [e^{j(\varphi_2+\varphi_3+\varphi_4)}, e^{j(\varphi_3+\varphi_4)}, e^{j(\varphi_2+\varphi_4)}, -e^{j(\varphi_4)}, e^{j(\varphi_2+\varphi_3)}, e^{j(\varphi_3)}, -e^{j(\varphi_2)}, 1]^T, \quad (\text{IV})$$

wherein \mathbf{s}_1 is an eight-dimensional vector representing one specific value combination out of a set of possible value combinations, which combinations are defined with (IIA, IIB). The number of possible value combinations for the first sub-modulation code equals $C_1 * C_2 * \dots * C_{i-1} * C_i * C_{i+1} * \dots * C_n$ wherein C_i is the number of elements of the i^{th} first set of the n first sets. In this example $n=3$, $C_1=2$, $C_2=1$, $C_3=2$ which yields 4 possible value combinations for the first sub-modulation code. In this example the number of first correlators M equals the number of possible value combinations in the first sub-modulation code.

The second sub-modulation code \mathbf{s}_2 is given by:

$$\mathbf{s}_2 = e^{j(\phi_1)}, \quad (\text{V})$$

wherein \mathbf{s}_2 is one specific value out of the set of possible values for the second sub-modulation code, wherein set is defined with (IIIA, IIIB). These possible values are depicted in figure 3. In this figure the values 42.1 up to 42.4 are depicted in the complex co-ordinate system 44 comprising a real axis Re 46 and an imaginary axis Im 48. The second sub-modulation code is a common modulation for all chips of the symbol (I).

It is stressed that the set CCK-symbols (I) as described hereinbefore is just one example. Various sets of symbols can be chosen with different numbers of chips per symbol and different modulation codes. However in the second modulation code always at least one value will be a complex number.

Each of the correlators 24.m ($m=1,2,\dots,M$) performs a correlation of the received signal 8 with one of the possible first sub-modulation codes \mathbf{c}_1 (IV). The number of correlators equals the number of first sub-modulation codes ($=C_1 * C_2 * \dots * C_{i-1} * C_i * C_{i+1} * \dots * C_n$). The correlation is performed as a matched filter, which means that the output signal of the correlator 24.m is given with the complex inner product:

$$\text{Cor}_m = \bar{\mathbf{s}}_1 \cdot \mathbf{r}, \quad (\text{VI})$$

wherein Cor_m is a complex scalar value, $\bar{\mathbf{s}}_1$ is the complex conjugated of the M -dimensional vector \mathbf{s}_1 , where \mathbf{s}_1 is the m^{th} first sub-modulation code of the first sub-modulation codes corresponding to the correlator 24.m, \mathbf{r} is the M -dimensional receive signal 8 and $\{\} \cdot \{\}$ is the complex inner product between

its arguments. Thus each of the first correlators 24.m yields a first correlation result 6.m ($m=1,2,...,M$). These M first correlation results are passed to the control-unit 20. Next the control-unit determines for each first correlation result 6.m the value of a function of the correlation result wherein the function is predetermined by the type of modulation of the second sub-modulation code. The type of modulation is defined with (IIIB) and (V). The function is a function of the real and/or imaginary parts of the first correlation result for selecting the value of phase-modulating elements of the first sub-modulation code which are incorporated in the symbol of the received signal. The function firstly leads the Maximum Likelihood detection symbol and secondly leads to a minimum of necessary processing time. For the chose type of second sub-modulation (defined with (IIIB) and (V)) this optimal function *Crit1* may be given with:

$$Crit1 = Max(|Re(Cor_m)|, |Im(Cor_m)|), \quad (VII)$$

wherein the function *Max()* selects the maximum value of its input arguments, the function $| \cdot |$ yields the absolute value of its input argument, the function *Re()* gives the real part of its complex input argument and the function *Im()* gives the imaginary part of its complex argument. The control-unit 20 subsequently controls the switch 34 in the first selection means 10 on the basis of the maximum value of the function (VII) in such a way that the corresponding first correlation result 6.m is selected by the first selection means 10 and passed to the second correlator-bank 12. Furthermore, the control unit selects the pre-determined phase modulating elements $e^{\hat{\phi}_2}, e^{\hat{\phi}_3}, e^{\hat{\phi}_4}$ (which correspond to the selected phase parameters $\hat{\phi}_2, \hat{\phi}_3, \hat{\phi}_4$ belonging to the first sub-modulation code which corresponds to the selected correlator) out of the set (II). A signal 28, comprising this first sub modulation code of correlator 6.m, is subsequently passed by the control unit 20 to the third selecting means 22.

The second correlator-bank 12 receives the selected first modulation signal 14 and subsequently performs a phase-modulation on this signal based on the second sub-modulation code (V). Each of the second correlators 16.k ($k=1,...,K$) performs a phase-modulation corresponding to one of the values of the second sub-modulation code c2 from (III) and (V). The result of these

phase-modulations are the second correlation results 16.k (k=1,...,K). In this example K=4. The second correlation results are passed to the second selection means 18. The selection means 22 select the pre-determined phase-modulating element $e^{\hat{\phi}_1}$ which corresponds to the second sub-modulation code of the correlator 16.k for which the following function *Crit2* is maximum:

$$Crit2 = (\text{Re}(Cor_m \cdot c2)), \quad (\text{VIII})$$

wherein Cor_m is the selected first correlation result and $c2$ is the second sub-modulation code from (V). The calculation of the function *Crit2* yields the second correlation results. It follows from (VIII) that the number of second correlation results equals the number of possible values of the phase parameter ϕ_1 of the second set (IIIB). The pre-determined phase-modulating element $e^{\hat{\phi}_1}$ of the second sub modulation code for which *Crit2* is maximum is the output signal 30.

The third selection means 22 receives a signal 30 comprising the selected predetermined phase modulating element $e^{\hat{\phi}_1}$ of the second set which yields the selected second sub-modulation result and a signal 28 comprising the selected predetermined phase modulating elements $e^{\hat{\phi}_2}, e^{\hat{\phi}_3}, e^{\hat{\phi}_4}$ of the first sets which yields the selected first sub-modulation result. On the basis of the signals 28 and 30 and the equation (I) the third selection means 22 can determine the detection symbol:

$$[e^{j(\hat{\phi}_1+\hat{\phi}_2+\hat{\phi}_3+\hat{\phi}_4)}, e^{j(\hat{\phi}_1+\hat{\phi}_3+\hat{\phi}_4)}, e^{j(\hat{\phi}_1+\hat{\phi}_2+\hat{\phi}_4)}, -e^{j(\hat{\phi}_1+\hat{\phi}_4)}, e^{j(\hat{\phi}_1+\hat{\phi}_2+\hat{\phi}_3)}, e^{j(\hat{\phi}_1+\hat{\phi}_3)}, -e^{j(\hat{\phi}_1+\hat{\phi}_2)}, e^{j(\hat{\phi}_1)}]^T \quad (\text{IX})$$

from the received signal 8.

The apparatus 2 according to the invention is not limited to the second sub modulation given with (V) for the set of values of the phase parameter ϕ_1 (IIIB). A variety of types of second sub modulation codes with a corresponding function *Crit1* can be used without departing from the scope of the invention. A few number of non-limiting examples are given below.

Example 1. The second sub modulation code $s2$ is defined as:

$$s2 = e^{j(\phi_1)}, \quad (\text{X})$$

for which the phase parameter ϕ_1 can take on the values in the following set:

$$\varphi_1 \in \left\{ \frac{\pi}{4}, \frac{3 \cdot \pi}{4}, \frac{5 \cdot \pi}{4}, \frac{7 \cdot \pi}{4} \right\}, \quad (\text{XI})$$

such that the number $K=4$ of second correlators in the second correlator bank

12. The corresponding function $Crit1$ is given with:

$$Crit1 = |\text{Re}(Cor_m)| + |\text{Im}(Cor_m)|, \quad (\text{XII})$$

wherein Cor_m is the selected first correlation result.

Example 2. The second sub modulation code $s2$ is defined as:

$$s2 = e^{j(\varphi_1)}, \quad (\text{XIII})$$

for which the phase parameter φ_1 can take on the values in the following set:

$$\varphi_1 \in \left\{ \frac{\pi}{4}, \dots, \frac{k \cdot \pi}{4}, \frac{(k+1) \cdot \pi}{4}, \dots, \frac{K \cdot \pi}{4} \right\}, \quad (\text{XIV})$$

such that the number $K=8$ of second correlators in the second correlator bank

12. The corresponding function $Crit1$ is given with:

$$Crit1 = \text{Max}(|\text{Re}(Cor_m)|, |\text{Im}(Cor_m)|, \frac{1}{2} \cdot \sqrt{2} \cdot (|\text{Re}(Cor_m)| + |\text{Im}(Cor_m)|)), \quad (\text{XV})$$

wherein Cor_m is the selected first correlation result.

Example 3. The second sub modulation code $s2$ is defined as:

$$s2 = e^{j(\varphi_1)}, \quad (\text{XVI})$$

for which the phase parameter φ_1 can take on the values in the following set:

$$\varphi_1 \in \left\{ \frac{\pi}{8}, \dots, \frac{k \cdot \pi}{8}, \frac{(k+1) \cdot \pi}{8}, \dots, \frac{16 \cdot \pi}{8} \right\} \quad (\text{XVII})$$

such that the the number $K=16$ of second correlators in the second correlator bank 12 and corresponding function $Crit1$ is given with:

$$\begin{aligned}
 Crit1 = & \text{Max}(|\text{Re}(Cor_m)|, |\text{Im}(Cor_m)|, \frac{1}{2} \cdot \sqrt{2 - \sqrt{2}} \cdot \\
 & \text{Max}(|\text{Re}(Cor_m)|, |\text{Im}(Cor_m)|) + \frac{1}{2} \cdot \sqrt{2 - \sqrt{2}} \cdot \text{Min} \\
 & \left(|\text{Re}(Cor_m)|, |\text{Im}(Cor_m)|, \frac{1}{2} \cdot \sqrt{2} \cdot (|\text{Re}(Cor_m)| + |\text{Im}(Cor_m)|) \right)),
 \end{aligned}
 \tag{XVIII}$$

wherein Cor_m is the selected first correlation result.

5 In accordance with the provisions of the patent statutes, the present invention has been described in what is considered to represent its preferred embodiments. However, it should be noted that the invention can be practised otherwise than as specifically illustrated and described without departing from its spirit or scope. For example,

10 it is possible to combine in the first and/or the second sub-modulation code a phase modulation with an amplitude modulation.